

GENERAL NOTES

FOUNDATIONS:
 THE SOIL BEARING VALUE SHALL NOT BE LESS THAN 2000 PSF. THE BEARING VALUE SHALL BE VERIFIED BY THE G.C. FOOTINGS SHALL BEAR IN UNDISTURBED SOIL. ALL 1/FOOT. ELEVATION ARE TO BE THE SAME UNLESS SHOWN OTHERWISE. IF ELEVATIONS ARE NOT THE SAME, SHADY VENT MUST BE INSTRUCTED OF ELEVATIONS IN WRITING WHEN CANOPY ORDER IS PLACED. FOOTINGS DESIGN COMPLIES W/ACI-318.

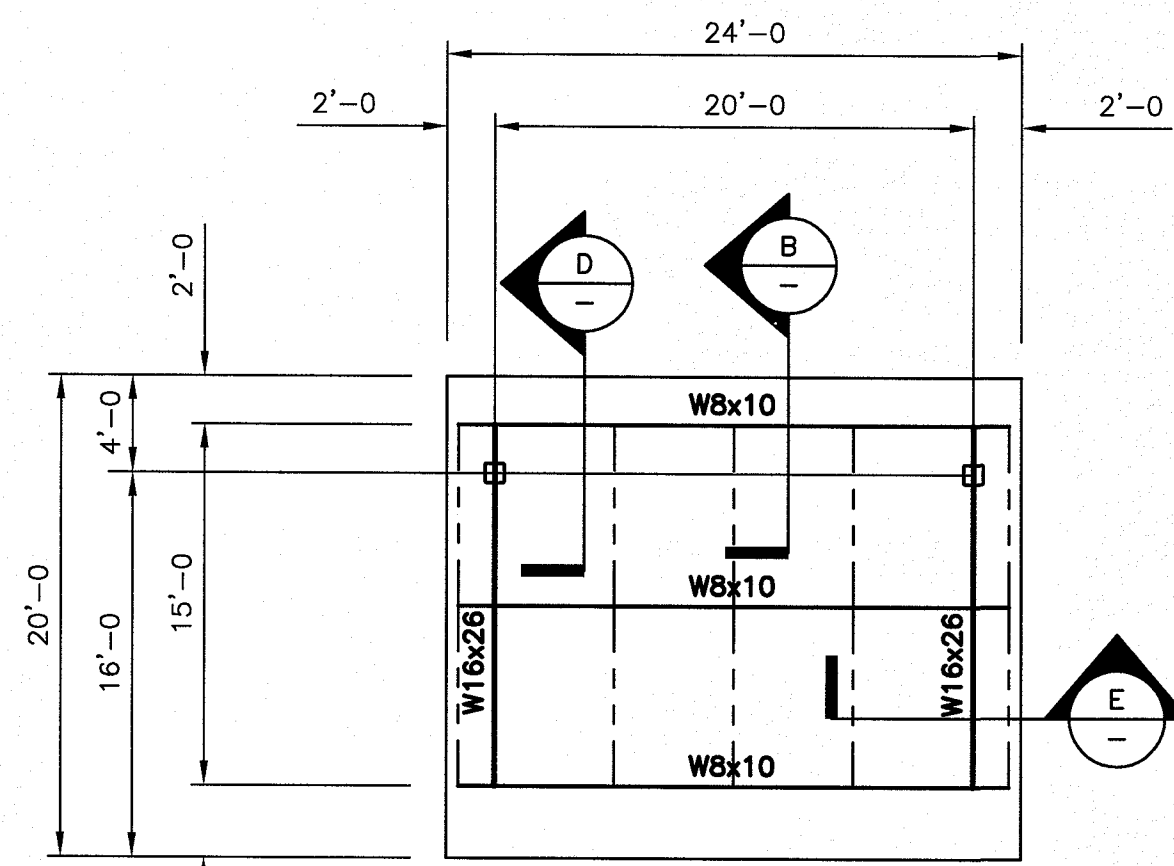
REINFORCING STEEL:
 ALL DEFORMED BARS SHALL COMPLY W/ASTM A615 FY=60 AND SHALL BE WIRE TIED AT ALL JOINTS. RUSTY, OILY, OR DIRTY STEEL SHALL NOT BE USED.

ANCHOR BOLTS:
 ANCHOR BOLTS MUST BE INSTALLED WITH A TEMPLATE AND WITHIN 1/8-INCH OF MEASUREMENTS OF THE BASE PLATE OR COLUMN WILL NOT FIT. CONCRETE CONTRACTOR IS RESPONSIBLE FOR RECESSING FOOTINGS 10 - INCHES BELOW FINISH GRADE AND FOR EXTENDING ANCHOR BOLTS 5 - INCHES ABOVE FOOTINGS IN ORDER FOR CANOPY TO TO ERECT PROPERLY. ANCHOR BOLTS SHALL BE ASTM A307.

CONCRETE:
 ALL CONCRETE SHALL BE 3000 PSI IN 28 DAYS. ALL CONC. SHALL BE PLACED IN ACCORDANCE WITH ACI-318.

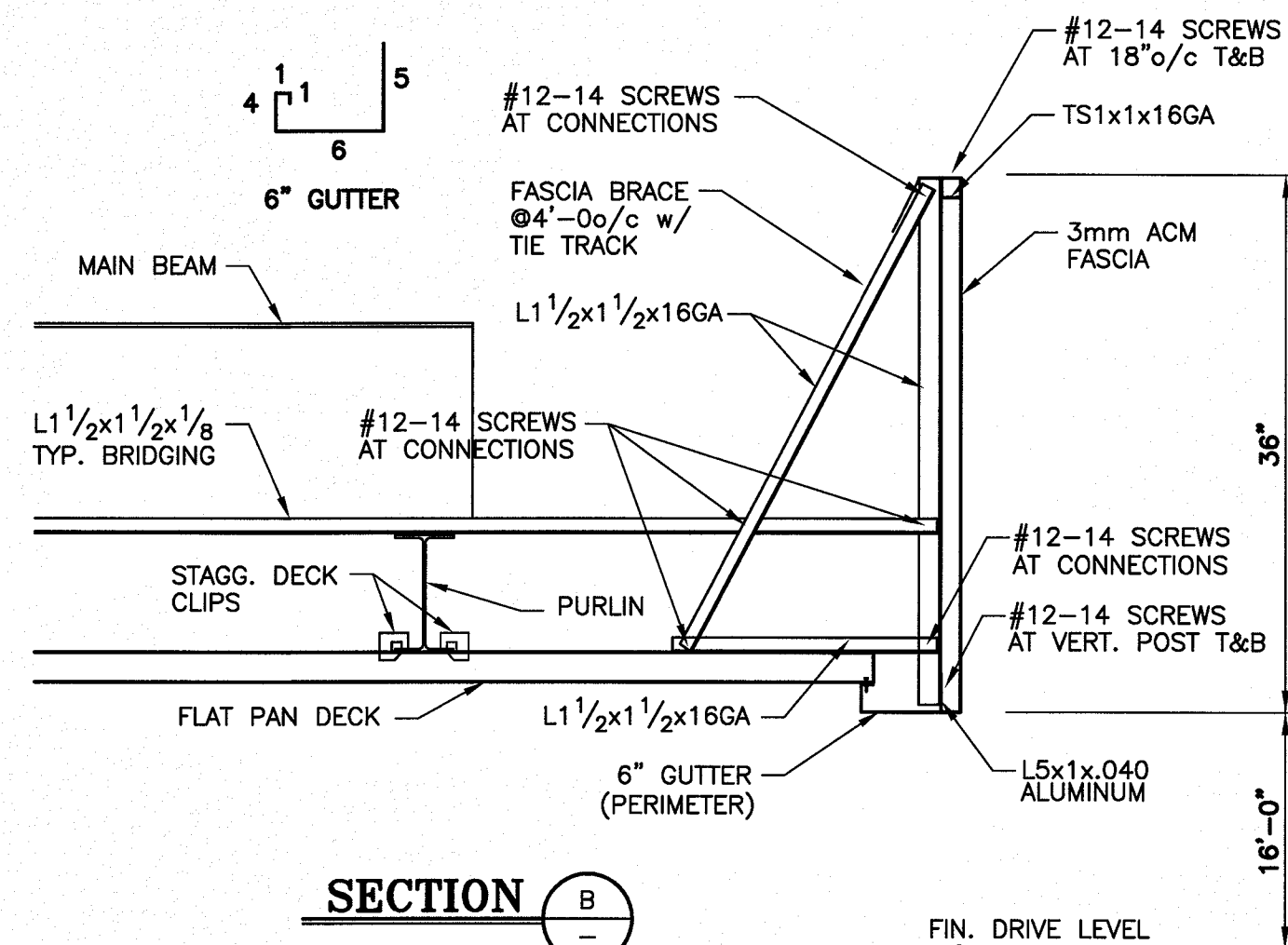
STRUCTURAL STEEL:
 ALL STRUCTURAL STEEL SHALL CONFORM TO ASTM A992 AND WITHIN 1/8-INCH OF MEASUREMENTS OF THE BASE PLATE OR COLUMN WILL NOT FIT. CONCRETE CONTRACTOR IS RESPONSIBLE FOR RECESSING FOOTINGS 10 - INCHES BELOW FINISH GRADE AND FOR EXTENDING ANCHOR BOLTS 5 - INCHES ABOVE FOOTINGS IN ORDER FOR CANOPY TO TO ERECT PROPERLY. ANCHOR BOLTS SHALL BE ASTM A307.

OTHER CONCRETE ITEMS:
 OTHER CONCRETE ITEMS SUCH AS DRIVE THRU SLAB, BUILDING SLAB, PERIMETER FOOTING, AND LOAD BEARING FOOTINGS NOT USED FOR THE CANOPY ARE TO BE AT THE SAME ELEVATION UNLESS SHOWN OTHERWISE. IF ELEVATIONS ARE TO VARY, SHADY VENT MUST BE INSTRUCTED OF ELEVATIONS IN WRITING WHEN ORDER IS PLACED.

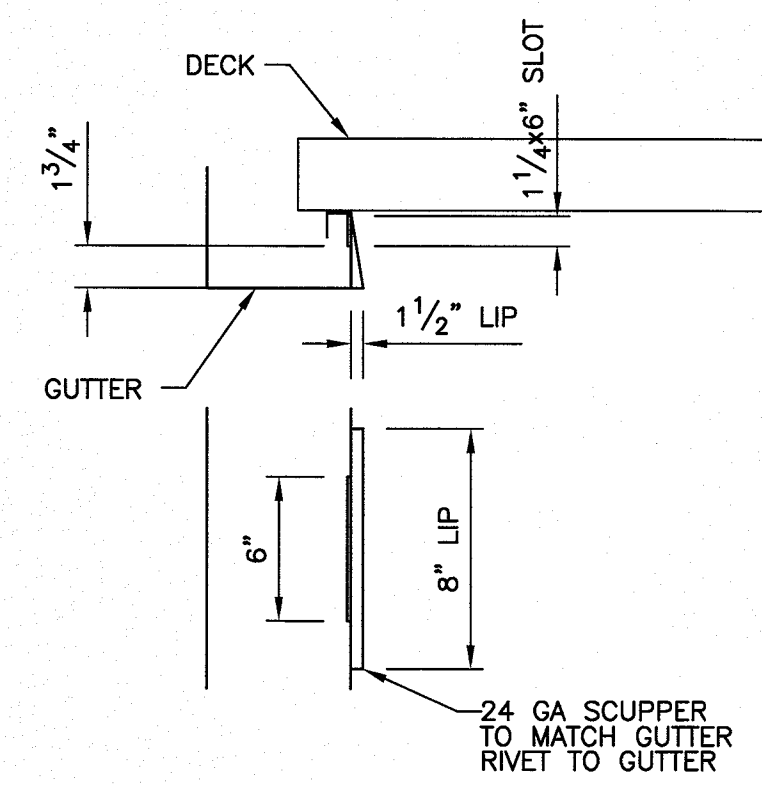


ROOF FRAMING PLAN

SCALE: 1/8" = 1'-0"

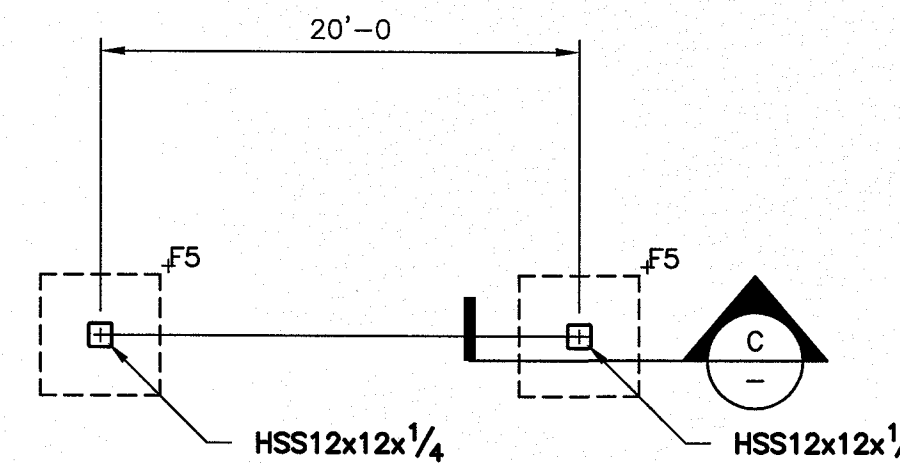


SECTION B



OVERFLOW

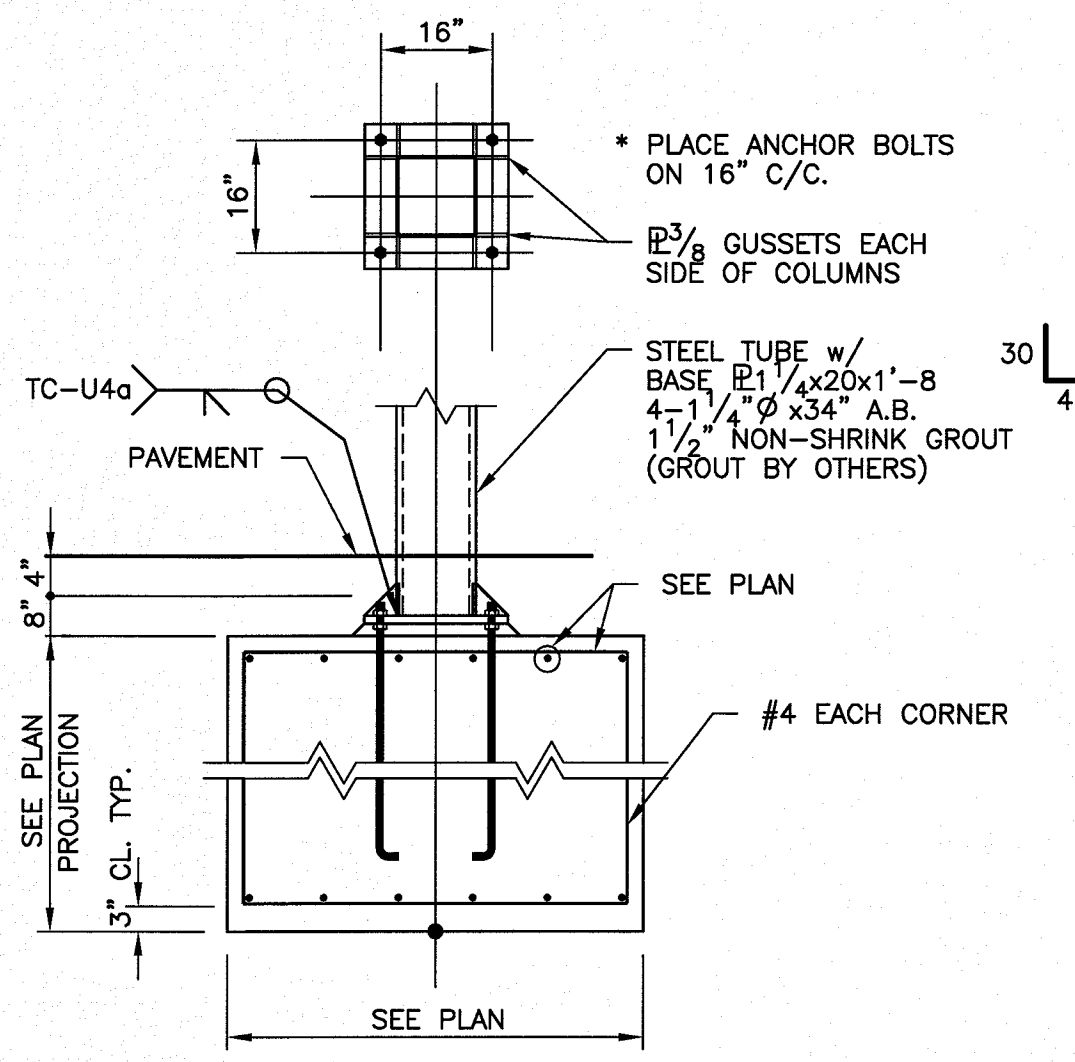
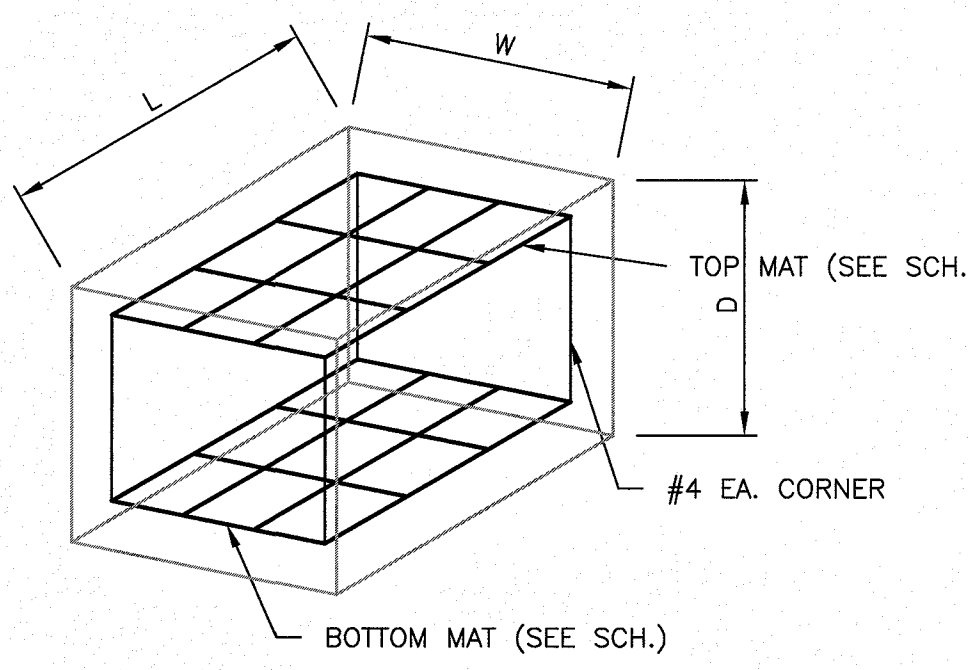
SCALE: 1 1/2" = 1'-0"



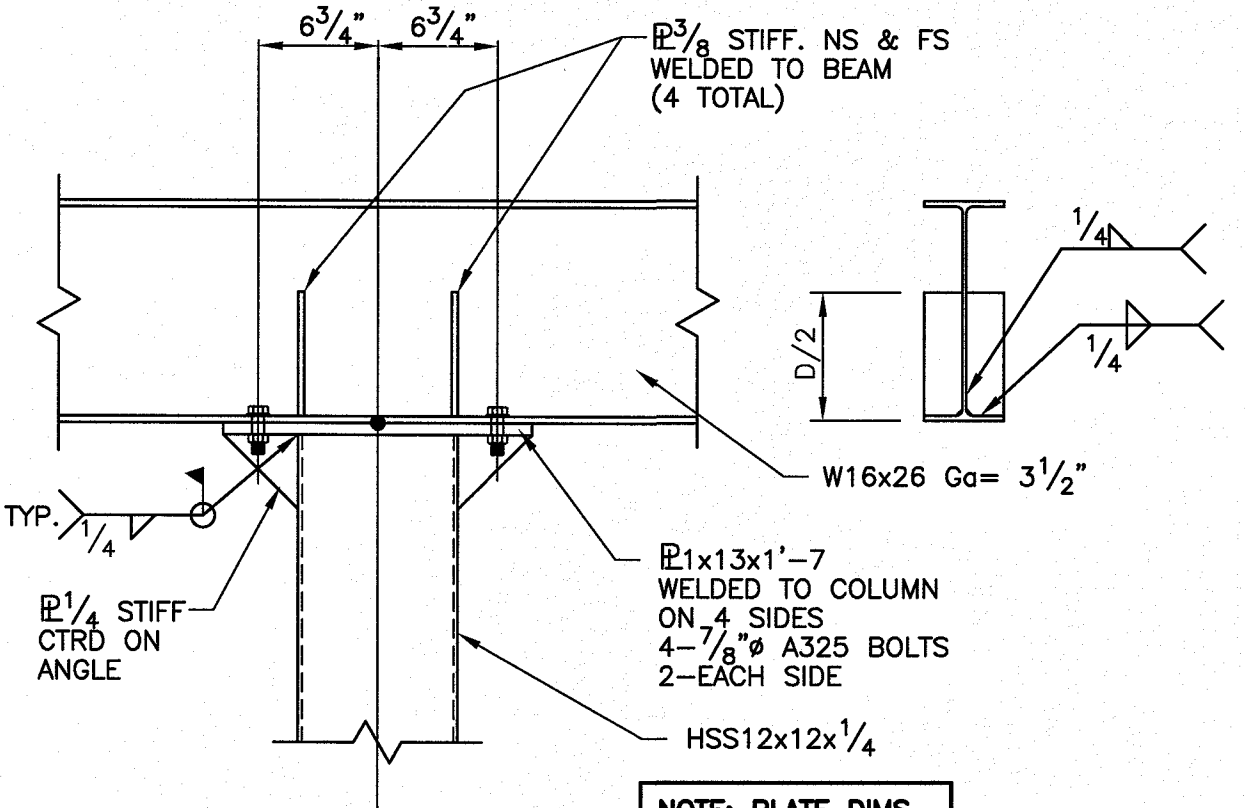
FOUNDATION PLAN

SCALE: 1/8" = 1'-0"

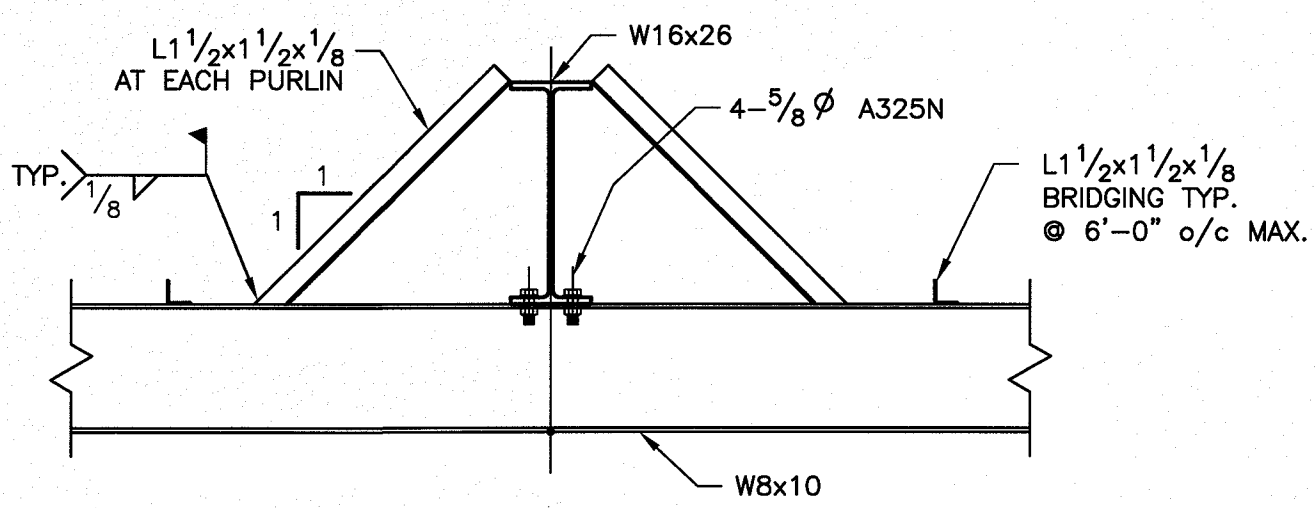
FOOTING SCHEDULE					
MARK	DIMENSIONS: LxWxD	#4 STEEL MAT TOP AND BOTTOM	#5 STEEL MAT TOP AND BOTTOM	#6 STEEL MAT TOP AND BOTTOM	REMARKS
F5	5'-0" x 5'-0" x 5'-0"	#4@8"o/c E.W.	#5@10"o/c E.W.	#6@12"o/c E.W.	#4, #5, AND #6 OPTIONS ALL STEEL SHOWN IS TO BE PLACED EACH WAY.



DETAIL C



SECTION D



SECTION E

NOTE: THIS CANOPY IS DESIGNED PER ASCE 7-10 SEE FIG. 27.4-4, UNBALANCED WIND LOAD

CASE A: 1.20(28.37) 0.30(7.09)

CASE B: -1.10(-26.01) -1.10(-2.36)

* CLEAR WIND FLOW

NOTES:
 1. THESE LOADS HAVE BEEN APPLIED TO STRUCTURE IN ACCORDANCE WITH ASCE 7-10, CHAPTER 2, 2.4.1 BASIC COMBINATIONS FOR ALLOWABLE STRESS
 2. THESE STEEL MEMBERS HAVE BEEN SIZED BASED ON ASD, AISC 14TH EDITION.
 3. ANALYSIS OF THIS STRUCTURE HAS BEEN ACCOMPLISHED USING THE LATEST GENERATION OF MATRIX BASED SOFTWARE.
 4. COLUMN SLENDerness FACTORS ARE BASED ON CHAPTER C, DIRECT ANALYSIS METHOD.
 Kx = 1.0
 Kz = 1.0
 5. BASES ARE FIXED.

STRUCTURE LOADS		
PARAMETER		CODE REFERENCE IBC 2012 w/ AMENDMENTS
DEAD LOAD	4.0 PSF	1606.1
LIVE LOAD	20.0 PSF (w/ APP. RED.)	1607.12.2.1
SNOW LOAD	5.0 PSF + DRIFTS	ASCE 7-10, PART 7.0
WIND SPEED	115.0 MPH 3 SEC. GUST	25.7 PSF ASCE 7, PART 26-29
CATEGORY II lw 1.0 EXP. C		
VERT. ROOF PRESSURE		
Case A Cnw Cnl	Case B Cnw Cnl	ASCE 7, FIG. 27.4-4
1.20(28.37) 0.30(7.09)	-1.10(-26.01) -1.10(-2.36)	
HORIZ. FASCIA PRESSURE EXP. C		
Case A & B Cfx	Cfx	ASCE 7, FIG. 29.4-1
1.85(47.50)	1.85(47.50)	
SEISMIC DATA		
SEISMIC DESIGN CATEGORY 11.6(1)(2) C		
.2 SEC. SPECTRUM RESPONSE, Ss 0.2000 FIG. 22.1		
1 SEC. SPECTRUM RESPONSE, S1 0.1000 FIG. 22.2		
LONG PERIOD TRANSITION PERIOD, Tl 12 FIG. 22-12		
RISK CATEGORY II TAB. 1.5-1		
SEISMIC FACTOR, Ie 1.00 TAB. 1.5-2		
SITE COEFFICIENT, Fa 1.60 TAB. 11.4-1		
SITE COEFFICIENT, Fv 2.40 TAB. 11.4-2		
SITE CLASSIFICATION D TAB. 20.3-1		
SITE ADJUSTMENT COEFFICIENT, Sms 0.3200 EQ. 11.4-1		
SITE ADJUSTMENT COEFFICIENT, Sm1 0.2400 EQ. 11.4-2		
DESIGN SPECTRAL RESPONSE, SDS 0.2134 EQ. 11.4-3		
DESIGN SPECTRAL RESPONSE, SD1 0.1601 EQ. 11.4-4		
W. Kips 03.05 12.8		
SEISMIC RESPONSE COEFFICIENT, Cs 0.1708 0.1708 12.8.1.1		
BASIC STRUCTURAL SYSTEM - SEISMIC RESISTING SYSTEM		
OPTIMUM MOMENT RESISTING FRAMES/CANTILEVERED. COL.		
RESPONSE MODIFICATION FACTOR, R 1.25 1.25 TAB. 12.2-1		
METHOD OF ANALYSIS - EQUIVALENT LATERAL FORCE V=CeW 12.8		
BASE SHEAR, Kips .65 .65 EQ. 12.8-1		

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20'x24' CANOPY

SHADY VENT

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 PHONE: 1-(770) 943-5977

NO.	DATE:	BY:
1	5/21/19	
2		
3		

CUSTOMER:	
SCALE: NOTED	DRAWN:
DATE:	APPROVED BY:
LOCATION:	REVISED:
DRAWING NO:	

CERTIFICATION